(E80 The Next Generation)

## LECTURE 8

## Modal Vibration

\*Basic Ideas:

Modal Analysis: Charaterization of vibrational.

mode shapes and corresponding frequencies of a physical system.

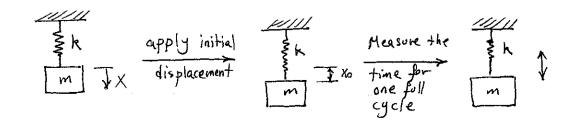
Properties of a system: Natural frequencies and modal shapes

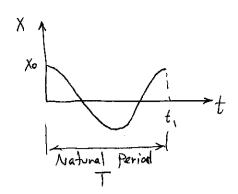
Dynamic vs. Static: Varying in time vs. constant in time

Dynamic loads: Loads applied dynamically (over time, varying)

Natural period of vibration of a structure:

Time required for the structure to undergo one complete cycle of free vibration.



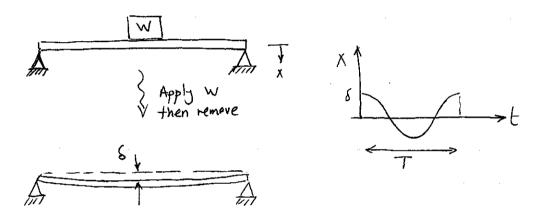




or can call it natural frequency

$$\omega = \frac{2\pi}{T}$$

Same for a structural component ...



If time variation of the load application is such that it is smaller or comparable to natural period of vibration of the structure, then your structure has no time to undergo a free vibration cycle and start to respond to the dynamic load.

the response associated to this type of loading is the dynamic response of the structure.

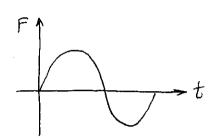
strains when dynamic loads are applied.

of Dynamic Loads

Various sources of dynamic loads can be named.

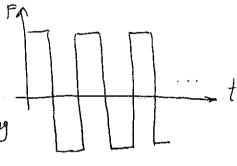
1) Simple Harmonic

example: Interaction of ocean waves with a structure.



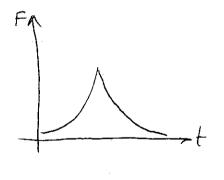
2) Periodic, non harmonic

Example: Loading and unloading a structure



3) Non-Periodic, Short duration

Example: Sudden impact to



4) Non-Peribdic, long duration

Example: Bridge with ongoing traffic

An important observation in dynamic loading is the fact that inertia plays an important note.

Analysis of Dynamic Loading:

How do you approach the problem of analyzing a structure with dynamic loading?

- a) Model your physical problem
  - Geometry
    - Kinematics
      - Material
      - Loading
- b) Derive governing equations (mostly differential equations)
- c) Solve the equations
- d) Interpret the results and refine and repeat!

What else can you do to characterize a structure?

Measurements! => Experimental studies to

validate a model or help develop a model.

\*A Simple model

Let's look at a very simple model that makes the building block of a lot of structural dynamics analysis tools ...

Free, undamped vibration of a spring-mass system

This is a single degree of freedom SDOF &k

system. m: mass k: spring anstant [m] TX(t)

we sav in E59 that this physical model

has a differential equation associated to it:

 $m\ddot{X} + kX = 0 \tag{1}$ 

with initial conditions of  $X(t=0)=X_0$  and  $X(t=0)=X_0$ 

we recall from \$59 that solution of (1)

amplitude pregruency

solution of (1)

is  $X(t) = X \sin(\omega t + \Phi)$  (2)

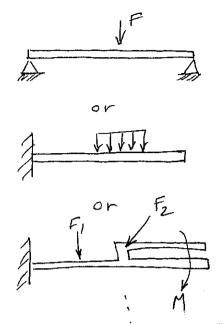
with  $X = \sqrt{X_0^2 + (\frac{\dot{X}_0^2}{\dot{w}})}$  and  $\Phi = \tan^{-1}(\frac{X_0 \, \omega}{\dot{X}_0})$  and  $\omega = \sqrt{k/m}$ 

So in a nut shell, if we manage to extend this ideal to a structural element, say a beam then we should be able to see how this structural element or even the structure as a whole responds to a free or forced (loaded) vibration (dynamic loading) case.

XBeams

Beams are one of the most important components in structural engineering. Examples of beams are bridges, walkways, rockets (?) and ....

Simple representation of beams



Some important properties and characteristics of a beam are:

- 1) Cross section Da Da O
- 2) Length and supports Fixed-Free, simply supported, ...
- 3) Loading

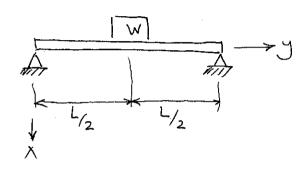
concentrated, listributed, dynamic static ...

4) Material

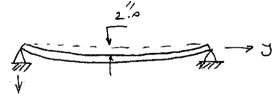
steel wood plastic, ...

Each of the above defines the model and paragreteurs needed to analyze the beam.

Let's study a beam problem that resembles our previous mass-spring, free vibration problem.



Consider the beam shown. Let's say the natural frequency of the beam is given to us as  $27.88 \text{ rad/s} \rightarrow \left(\frac{27.88}{27} - 444\right)$ As a result of applying load W, this beam deflects



If load w is released at -3.0 insec, we want to find out the amplitude of the oscillation for the beam.

If we model our beam as a mass-spring system then

$$X(+) = X \sin(\omega + + +)$$
  $\omega = 27.88$  rad/sec  
 $X = \sqrt{X_0^2 + (\frac{X_0}{\omega})^2} = \sqrt{2.0 + (\frac{3.0}{27.88})^2} = 2.005$   $X_0 = -3.0$  in/sec

$$X(t) = X w \cos(\omega t + \phi)$$
  $\frac{X max}{x} = X w max = X w max = 2.005 x 27.88 = 55.9 is  $\frac{i\eta}{s}$$ 

$$\dot{X}(t) = -X\omega^2 \sin(\omega t + \Phi) \frac{\dot{X}_{max}}{\dot{X}_{max}} \dot{X}_{max} = X\omega^2 = 1558.48 \text{ in/sec}^2$$

$$\dot{\Phi} = tan^{-1} \left( \frac{\dot{X}_{o}\omega}{\dot{X}_{o}} \right) = tan^{-1} \left[ \frac{2 \times 27.88}{-3} \right] = 273^{\circ}$$

Having X, X, X and \$\phi\$ one can predict how this beam oscillates and what magnitudes of displacement, velocity and ... to expect. These can help design a component within the design requirements and limitations.

Equivalent stiffness

One important observation is w of the

system which was known at the beginning.

we know that  $w = \sqrt{\frac{R}{m}}$  so what is k for

a beam?

we call k the equivalent stiffness of the beam.

Key depends on sevenal factors:

Cross section say I

Length \_\_\_\_ L

Elasticity \_\_\_ E

For example discussed

 $R_{eq} = \frac{192 EI}{L^3}$ 

The important question, now that we saw the analogy between mass-spring and beams is how to model a dynamic load response of a beam?

In other words, how do you derive appropriate differential equations?

Let's look at a problem that pretty much resembles what you will be testing in the lab. We hope to extend the results obtained for this model to that of a rocket structure (hollow cylinder).

\* Transverse vibration of a pretensioned cable (e.g. Guitar string)

Consider a uniform, elastic cable

with mass ber unit length Y.

Let's apply a tension T between

the two fixed points.

 $\frac{1}{\sqrt{10+\frac{30}{30}}}$ 

For small deflections use = ma

Tsin 
$$\left(\theta + \frac{\partial \theta}{\partial x} dx\right)$$
 Tsin  $\theta = \frac{y}{y} dx$   $\frac{\partial^2 y}{\partial t^2}$   
Force from Force from the left side acceleration

$$\frac{\partial \theta}{\partial x} = \frac{x}{T} \frac{\partial^2 y}{\partial t^2}$$

since 
$$\theta = \frac{\partial y}{\partial \dot{x}}$$
 is the slope of the cable,

$$\Rightarrow \frac{\partial^2 y}{\partial x^2} = \frac{1}{C^2} \frac{\partial^2 y}{\partial t^2} \quad \text{vith} \quad C = \sqrt{\frac{T}{Y}} \tag{*}$$

where c is the velocity of the wave propagation along the cable.

Solving equation (\*) requires the use of method of separation of variables which is a classical mathematic topic. Obtaining the solution results in  $y(x,t) = \left( C_1 \sin \frac{\omega}{C} x + C_2 \cos \frac{\omega}{C} x \right) \left( A \sin \omega t_+ B \cos \omega t \right)$ Use boundary anditions of y(0,t) = y(L,t) = 0to get  $C_2 = 0$ 

 $\Rightarrow J(X,t) = (A \sin \omega t + B \cos \omega t) C_1 \sin \omega x$ and for X = L  $\Rightarrow J(0,t) = 0 \Rightarrow C_1 \sin \omega L = 0$ if  $C_1 = 0 \Rightarrow trivial$  solution, no meaningful result  $\Rightarrow \sin \omega L = 0 \text{ is considered the correct chaice.}$ 

$$\Rightarrow \omega_n = \frac{n\pi c}{L} / c = \sqrt{\frac{T}{Y}} \Rightarrow \omega_n = \frac{n\pi}{L} \sqrt{\frac{T}{Y}} = \frac{n\pi}{L} \sqrt{\frac{T}{Y}}$$

Each we corresponds to a normal mode vibration having a

mode shape In with a sinuspidal distribution

add all add all 
$$y(x)t = \sum_{n=1}^{\infty} (A_n \sin w_n t + B_n \cos w_n t) \sin \frac{w_n}{c} x$$

where  $A_n = AC_1$  and  $B_n = BC_1$ 

Now with initial conditions,  $y(x,0) = % \sin \frac{\pi}{L} x$ 

and zero velocity;  $\frac{\partial \mathcal{J}(x,0)}{\partial t} = 0$ 

$$\Rightarrow$$
 An=0 and B<sub>1</sub>= $\frac{1}{2}$ , B<sub>n=0</sub> for  $\frac{1}{2}$ 

$$= y(x,t) = \sum_{n=1}^{\infty} y_n \cos \omega_n t \sin \frac{n\pi}{L} x$$

$$= \int_{0}^{\infty} y(x,t) = \sum_{n=1}^{\infty} y_n \cos \omega_n t \sin \frac{n\pi}{L} x$$

Displacement of the string as a function of space of time



what this equation tells us is that our string can oscillate with shapes formed by adding infinite numbers of individual modes.

Say n=1 only  $y(x,t) = \frac{y}{cos} \omega_1 t \sin \frac{\pi}{L} x$ 

y 1 X=0 X=L

If n=2

 $y(x, t) = \frac{1}{2} \cos \omega_1 t \sin \frac{\pi}{L} x + \frac{1}{2} \cos \omega_2 t \sin \frac{2\pi}{L} x$ 

Now with we and sin 27 X, 3 locations yield y=0

X=0, X=L and  $X=\frac{L}{2}$  so mode 2 shape should

look like this.

while mode n=1 is the same as before, mode n=2 exhibits a different shape mode.

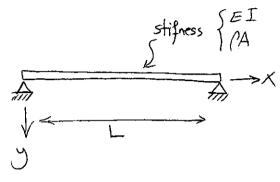
Finally let's extend the idea to a transverse vibration of uniform beams...

This time replace the string with a bean shown below:

(This can be your rocket !!)

EI is a measure of how stiff the beam is and its area

PA is for inertia and naterial



bean bean

we skip the mathematical details of the solution and write the expression:

$$|\mathcal{J}(x,t)| = \frac{\infty}{\sum_{n=1}^{\infty} (A_n \sin \omega_n t + B_n \cos \omega_n t) \sin \frac{n\pi x}{L}|$$

-> Recall the string problem on page 13!

Our goal in the lab is to find was

$$\omega_n = (\beta_n L)^2 \sqrt{\frac{ET}{\beta A L^4}}$$

See other notes for free-free solution!

note EI and PA and L
playing major role in
frequency of oscillation!

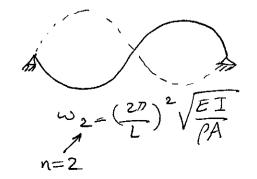
where  $B_n$  for  $\frac{n\pi}{L}$  beam is  $\frac{n\pi}{L}$ 

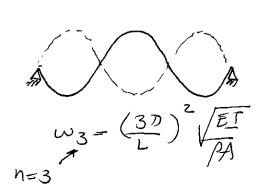
## X Summary:

We will be using tap test as excitation of the beam (Rocket body) and will measure response of the beam (with accelerameters mounted on the rocket) in time and frequency domains.

By obtaining all response frequencies (wn's) we can find out which modes (y(x,t);) have been excited as the result of our test. knowing theoretical values of wn enables us to compare the experimental results with analytical results.

Example of normal modes for the bean:





## \* Goals for experiments

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\*You will be using LabVIEW, DAQ and

RDAS systems to acquire data and

present them in different domains (time, frequency)

\*You will be given basic dimensions, properties and

other necessary physical parameters to compute the

theoretical frequencies of the free-free beam

test.