





#### Inertial Measurement



Feb. 17, 2015 Christopher M.

http://www.volker-doormann.org/physics.htm





# Where was the rocket?







# <u>Outline</u>

- Sensors
- Representations
- State Estimation
- Example Systems
- Bounding with KF





# <u>Outline</u>

- Sensors
  - People
  - Accelerometers
  - Gyroscopes
- Representations
- State Estimation
- Example Systems
- Bounding with KF





People

http://en.wikipedia.org/wiki/File:Bigotolith.jpg







Accelerometers

$$a = k x / m$$







- Accelerometers
  - The accelerometers are typically MEMS based
  - $\square$  They are small cantilever beams (~100 µm)







- Gyroscopes (original)
  - Mounted on two nested gimbals, the spinning wheel of the gyroscope is free to take any orientation.



High spin rate leads to high angular momentum







http://www.youtube.com/watch?v=cquvA\_lpEsA





- Gyroscopes (original)
  - The gyroscope resists any change of orientation caused by external torques, due to the principle of conservation of angular momentum.
  - The orientation of the gyroscope remains nearly fixed, regardless of any motion of the platform.







- Gyroscopes (original)
  - Gyroscope orientation can be obtained by measuring the angles between adjacent gimbals.







- MEMS (Microelectromechanical Systems) Gyroscopes
  - Two masses oscillate back and forth from the center of rotation with velocity v.
  - □ A rotation will cause a Coriolis force in this coordinate frame.







- MEMS Gyroscopes
  - $\square$  Their deflection *y* is measured, to establish a force

$$F_{Coriolis} = k y$$

• The acceleration is obtained since the mass is known  $-2m |\mathbf{\Omega} \times \mathbf{v}| = F_{Coriolis}$ 





- Inertial Measurement Units
  - a 3 Accelerometers
  - Gyroscopes
  - a 3 Magnetometers(?)



www.barnardmicrosystems.com





Inertial Measurement Units







# <u>Outline</u>

- Sensors
- Representations
  - Cartesian Coordinate Frames
  - Transformations
- State Estimation
- Example Systems
- Bounding with KF







zł

0

X

v

(x,y,z)

Z

- Cartesian
  Coordinate Frames
  - We can represent the 3D position of a vehicle with the vector

$$\mathbf{r} = [x y z]$$





# **Representations**

- Euler Angles
  - We can represent the 3D orientation of a vehicle with the vector

$$\boldsymbol{\phi} = [\alpha \beta \gamma]$$

Yaw -  $\alpha$ Pitch -  $\beta$ Roll -  $\gamma$ 







- Where do we place the origin?
  - We can fix the origin at a specific location on earth, e.g. a rocket's launch pad.
  - This is called the **global** or inertial coordinate frame







# **Representations**

- Where do we place the origin?
  - We can ALSO fix the origin on a vehicle.
  - This is called the **local** coordinate frame







# **Representations**

- Where do we place the origin?
  - We must differentiate between these two frames.
  - What is the real difference between these two frames?
  - A Transformation consisting of a rotation and translation







- Transformations
  - The rotation can be about 3 axes (i.e. the roll, pitch, yaw)







- Transformations
  - The rotation can be about 3 axes (i.e. the roll, pitch, yaw)







- Transformations
  - The translation can be in three directions







# **Representations**

- Rotations
  - In 2D, it is easy to determine the effects of rotation on a vector



$$\mathbf{q}_2 = \begin{pmatrix} \cos(\alpha) & -\sin(\alpha) \\ \sin(\alpha) & \cos(\alpha) \end{pmatrix} \mathbf{q}_1$$

$$= \mathbf{R}(\alpha) \mathbf{q}_{1}$$





- Rotations
  - We want to determine the rocket acceleration with respect to the global frame







# **Representations**

- Rotations
  - We can measure rocket acceleration in the local frame.







# **Representations**

- Rotations
  - To get the acceleration vector in the Global frame, we rotate the acceleration vector in the local frame by α - the rotation angle between frames







- Rotations
  - Here, we want to determine how acceleration in one frame relates to acceleration in another.

$$\begin{bmatrix} a_{x,G} \\ a_{y,G} \end{bmatrix} = \begin{bmatrix} \cos(\alpha) & -\sin(\alpha) \\ \sin(\alpha) & \cos(\alpha) \end{bmatrix} \begin{bmatrix} a_{x,L} \\ a_{y,L} \end{bmatrix}$$

$$\mathbf{a}_G = \mathbf{R}(\alpha) \ \mathbf{a}_L$$







- Rotations
  - Here, we want to determine how acceleration in one frame relates to acceleration in another.

$$\begin{bmatrix} a_{x,G} \\ a_{y,G} \end{bmatrix} = \begin{bmatrix} \cos(\alpha) & -\sin(\alpha) \\ \sin(\alpha) & \cos(\alpha) \end{bmatrix} \begin{bmatrix} a_{x,L} \\ a_{y,L} \end{bmatrix}$$



$$\mathbf{a}_G = \mathbf{R}(\alpha) \ \mathbf{a}_L$$





≯

 $Y_G$ 

# <u>Representations</u>

- Rotations
  - In 3D, we can use similar rotation matrices

 $Z_G \uparrow$ 





#### **Representations**

$$\mathbf{R}_{\mathbf{x}}(\gamma) = \begin{pmatrix} 1 & 0 & 0 \\ 0 & \cos(\gamma) & -\sin(\gamma) \\ 0 & \sin(\gamma) & \cos(\gamma) \end{pmatrix}$$
$$\mathbf{R}_{\mathbf{y}}(\beta) = \begin{pmatrix} \cos(\beta) & 0 & \sin(\beta) \\ 0 & 1 & 0 \\ -\sin(\beta) & 0 & \cos(\beta) \end{pmatrix}$$
$$\mathbf{R}_{\mathbf{z}}(\alpha) = \begin{pmatrix} \cos(\alpha) & -\sin(\alpha) & 0 \\ \sin(\alpha) & \cos(\alpha) & 0 \\ 0 & 0 & 1 \end{pmatrix}$$





Rotations

□ For 3 rotations, we can write a general Rotation Matrix

 $\mathbf{R}(\alpha, \beta, \gamma) = \mathbf{R}_{\mathbf{z}}(\alpha) \ \mathbf{R}_{\mathbf{y}}(\beta) \ \mathbf{R}_{\mathbf{x}}(\gamma)$ 

 Hence, we can rotate any vector with the general Rotation Matrix

$$\mathbf{q}_2 = \mathbf{R}(\alpha, \beta, \gamma) \mathbf{q}_1$$





- Rotations
  - Hence, we can rotate any acceleration vector in a local frame through roll, pitch, yaw angles to get the corresponding acceleration vector in the global frame

$$\mathbf{a}_{G} = \mathbf{R}(\alpha, \beta, \gamma) \mathbf{a}_{L}$$





# <u>Outline</u>

- Sensors
- Representations
- State Estimation
  - Updating  $\mathbf{R}(t)$
  - Updating  $\mathbf{r}(t)$
  - Pseudo Code
- Example Systems
- Bounding Errors with KF





- Strapdown Inertial Navigation
  - Our IMU is fixed to the local frame
  - We care about the state of the vehicle in the **global** frame







#### Given: $\omega_L(t) = [\omega_{x,L}(t) \omega_{y,L}(t) \omega_{z,L}(t)]$

Find:  $\mathbf{R}(t)$ 





• Lets define the rotational velocity matrix based on our gyroscope measurements  $\omega_L = [\omega_{x,L}(t) \ \omega_{y,L}(t) \ \omega_{z,L}(t)]$ 

$$\Omega(t) = \begin{pmatrix} 0 & -\omega_z(t) & \omega_y(t) \\ \omega_z(t) & 0 & -\omega_x(t) \\ -\omega_y(t) & \omega_x(t) & 0 \end{pmatrix}$$





# Updating $\mathbf{R}(t)$

 It can be shown that the vehicle rotating with velocity Ω(t) for δt seconds will (approximately) yield the resulting rotation Matrix R(t+δt):

 $\mathbf{R}(t+\delta t) = \mathbf{R}(t) \left[ \mathbf{I} + \mathbf{\Omega}(t)\delta t \right]$ 





Given: 
$$a_{L} = [a_{x,L} a_{y,L} a_{z,L}]$$
  
**R**(*t*)

Find: 
$$\mathbf{r}_{G} = [x_{G} \ y_{G} \ z_{G}]$$











• First, convert to global reference frame

 $\mathbf{a}_{\boldsymbol{G}}(t) = \mathbf{R}(t) \ \mathbf{a}_{\boldsymbol{L}}(t)$ 

Second, remove gravity term

 $\mathbf{a}_{\mathbf{G}}(t) = \begin{bmatrix} a_{x,\mathbf{G}}(t) & a_{y,\mathbf{G}}(t) & a_{z,\mathbf{G}}(t) - g \end{bmatrix}$ 





Third, integrate to obtain velocity

$$\mathbf{v}_{G}(t) = \mathbf{v}_{G}(0) + \int_{0}^{t} \mathbf{a}_{G}(\tau) d\tau$$

• Fourth, integrate to obtain position

$$\mathbf{r}_{\boldsymbol{G}}(t) = \mathbf{r}_{\boldsymbol{G}}(0) + \int_{0}^{t} \mathbf{v}_{\boldsymbol{G}}(\tau) d\tau$$





# Updating $\mathbf{r}(t)$

Third, integrate to obtain (approximate) velocity

$$\mathbf{v}_{\mathbf{G}}(t+\delta t) = \mathbf{v}_{\mathbf{G}}(t) + \mathbf{a}_{\mathbf{G}}(t+\delta t) \,\delta t$$

Fourth, integrate to obtain (approximate) position

$$\mathbf{r}_{\mathbf{G}}(t+\delta t) = \mathbf{r}_{\mathbf{G}}(t) + \mathbf{v}_{\mathbf{G}}(t+\delta t) \,\delta t$$





for t = 0 to maxTime {  $\omega(t) = \dots$   $\alpha_L(t) = \dots$   $R(t) = \dots$   $\alpha_G(t) = \dots$   $\alpha_G(t) = \dots //$  subtract gravity  $v_G(t) = \dots$  $r_G(t) = \dots$ 

}

. . .





- What about Errors?
  - We could use Error Propagation

$$\mathbf{r}_{G}(t+\delta t) = \mathbf{r}_{G}(t) + \mathbf{v}_{G}(t+\delta t) \,\delta t$$

• So

$$\mathbf{e}_{\mathbf{r}G}(t+\delta t)^{2} = \left(\frac{d\mathbf{r}_{G}(t+\delta t)}{d\mathbf{r}_{G}(t)}\right)^{2} \mathbf{e}_{\mathbf{r}G}(t)^{2} + \left(\frac{d\mathbf{r}_{G}(t+\delta t)}{d\mathbf{v}_{G}(t+\delta t)}\right)^{2} \mathbf{e}_{\mathbf{v}G}(t+\delta t)^{2}$$





}





What is bad about the second term?

$$\mathbf{e}_{\mathbf{r}G}(t+\delta t)^{2} = \left(\frac{d\mathbf{r}_{G}(t+\delta t)}{d\mathbf{r}_{G}(t)}\right)^{2} \mathbf{e}_{\mathbf{r}G}(t)^{2} + \left(\frac{d\mathbf{r}_{G}(t+\delta t)}{d\mathbf{v}_{G}(t+\delta t)}\right)^{2} \mathbf{e}_{\mathbf{v}G}(t+\delta t)^{2}$$





- Errors accumulate!
  - Each error is a function of the error from the previous time step

$$\mathbf{e}_{\mathbf{r}G}(t+\delta t)^{2} = \left(\frac{d\mathbf{r}_{G}(t+\delta t)}{d\mathbf{r}_{G}(t)}\right)^{2} \mathbf{e}_{\mathbf{r}G}(t)^{2} + \left(\frac{d\mathbf{r}_{G}(t+\delta t)}{d\mathbf{v}_{G}(t+\delta t)}\right)^{2} \mathbf{e}_{\mathbf{v}G}(t+\delta t)^{2}$$

• For example

 $\mathbf{e}_{\mathbf{r}\mathbf{G}}(t) = f(\mathbf{e}_{\mathbf{r}\mathbf{G}}(t-\delta t), \ \mathbf{e}_{\mathbf{v}\mathbf{G}}(t))$  $\mathbf{e}_{\mathbf{r}\mathbf{G}}(t-\delta t) = f(\mathbf{e}_{\mathbf{r}\mathbf{G}}(t-2\delta t), \ \mathbf{e}_{\mathbf{v}\mathbf{G}}(t-\delta t))$ 





# <u>Outline</u>

- Sensors
- Representations
- State Estimation
- Example Systems
  - □ LN-3
  - The Jaguar
- Bounding Errors with KF





- LN-3 Inertial Navigation System
  - Developed in 1960's
  - Used gyros to help steady the platform
  - Accelerometers on the platform were used to obtain accelerations in global coordinate frame
  - Accelerations (double) integrated to obtain position







- The Jaguar Lite
  - Equipped with an IMU, camera, laser scanner, encoders, GPS



Power Switch





- The Jaguar Lite
  - GUI provides acceleration measurements







- Question:
  - Can we use the accelerometers alone to measure orientation?







# <u>Outline</u>

- Sensors
- Representations
- State Estimation
- Example Systems
- Bounding Errors with KF
  - Exteroceptive Sensing
  - Fusing measurements





- Exteroceptive sensors
  - Drift in inertial navigation is a problem
  - We often use exteroceptive sensors which measure outside the robot – to bound our errors
  - Examples include vision systems, GPS, range finders







- Exteroceptive sensors
  - We can fuse measurements, e.g. integrated accelerometer measurements and range measurements, by averaging.
  - □ For example, consider the 1D position estimate of the jaguar.

$$x = 0.5 (x_{IMU} + (x_{wall} - x_{laser}))$$

 $x_{IMU}$  is the double integrated IMU measurement  $x_{wall}$  is the distance from the origin to the wall  $x_{laser}$  is the central range measurement





- Exteroceptive sensors
  - Lets weight the average, where weights reflect measurement confidence

$$x = \frac{w_{IMU}x_{IMU} + w_{laser}(x_{wall} - x_{laser})}{w_{IMU} + w_{laser}}$$





- Exteroceptive sensors
  - This leads us to a 1D Kalman Filter

$$x_t = x_{IMU,t} + K_t [(x_{wall} - x_{laser,t}) - x_{IMU,t}]$$

$$K_{t} = \frac{\sigma^{2}_{IMU}}{\sigma^{2}_{IMU} + \sigma^{2}_{laser}}$$

$$\sigma_x^2 = (1 - K_t) \sigma_{IMU}^2$$





#### IMU

- Higher sampling rate
- Small errors between time steps (maybe centimeters)
- Uncertainty increases
- Large build up over time (unbounded)
- GPS
  - Lower sampling rate
  - Larger errors(maybe meters)
  - Uncertainty decreases
  - No build up (bounded)







http://www.youtube.com/watch?v=l\_cCeGm4x4c











Shark Tagging







#### Result: Boat Track







