

1-D Analytical Model

Assume that the thrust is constant from $t = 0$ to $t = t_1$ at a value of T_1 . The initial velocity is $v_0 = 0$. Then from $t = t_1$ to $t = t_2$ the thrust is constant at a value of T_2 . Finally, from $t = t_2$ to $t = t_d$ (when the parachute deploys), the thrust is constant at $T_0 = 0$. For the drag force we assume a constant drag coefficient, C_D . The drag force is then

$$F_D = \frac{1}{2} C_D A_p \rho v^2. \quad (1.1)$$

The force balance on the rocket is

$$ma = T_x - \frac{1}{2} C_D A_p \rho v |v| - mg \quad (1.2)$$

Where x is 1, 2, or 0 and the absolute value sign takes care of whether the rocket is rising or falling. Division through by the mass gives

$$a = \frac{T_x}{m} - g - \frac{1}{2} C_D A_p \frac{\rho}{m} v |v| \quad (1.3)$$

To make computations easier, we'll calculate the velocity when the acceleration is 0. With no thrust, the velocity is the terminal velocity, v_t . For the thrust case, we'll call it the maximum velocity, v_{\max} . The terminal velocity is

$$v_t = \sqrt{\frac{2mg}{\rho C_D A_p}} \quad (1.4)$$

And the maximum velocity is

$$v_{\max} = \sqrt{\frac{2(T_x - mg)}{\rho C_D A_p}} \quad (1.5)$$

The acceleration can then be written as

$$a = \left(\frac{T_x - mg}{m} \right) \left(1 - \frac{v^2}{v_{\max}^2} \right) = b \left(1 - \frac{v^2}{v_{\max}^2} \right). \quad (1.6)$$

Written in differential equation form it becomes

$$\frac{dv}{dt} = b \left(1 - \frac{v^2}{v_{\max}^2} \right) \quad (1.7)$$

Which is separable to

$$\frac{dv}{\left(1 - \frac{v^2}{v_{\max}^2}\right)} = b dt. \quad (1.8)$$

Integrating

$$\int_{v_0}^{v_f} \frac{dv}{\left(1 - \frac{v^2}{v_{\max}^2}\right)} = b \int_{t_0}^{t_f} dt \quad (1.9)$$

$$v_{\max} \tanh^{-1} \frac{v}{v_{\max}} \Big|_{v_0}^{v_f} = b(t_f - t_0) \quad (1.10)$$

Or

$$v_f = v_{\max} \tanh \left[\frac{b}{v_{\max}} (t_f - t_0) + \tanh^{-1} \frac{v_0}{v_{\max}} \right] \quad (1.11)$$

However, if v_0 is greater than v_{\max} , then the integral becomes

$$v_{\max} \coth^{-1} \frac{v}{v_{\max}} \Big|_{v_0}^{v_f} = b(t_f - t_0) \quad (1.12)$$

Or

$$v_f = v_{\max} \coth \left[\frac{b}{v_{\max}} (t_f - t_0) + \coth^{-1} \frac{v_0}{v_{\max}} \right] \quad (1.13)$$

The physical difference is that if v_0 is less than v_{\max} , the rocket will accelerate, but if v_0 is greater than v_{\max} , the rocket will decelerate.

v_0 and t_0 are initial conditions, but v_f is the velocity at t_f , which is an arbitrary time within the specified interval (we could have used dummy variables and integrated to t). We can therefore write for $v_0 < v_{\max}$,

$$\frac{dx}{dt} = v_{\max} \tanh \left[\frac{b}{v_{\max}} (t - t_0) + \tanh^{-1} \frac{v_0}{v_{\max}} \right] \quad (1.14)$$

Which is again separable into

$$dx = v_{\max} \tanh \left[\frac{b}{v_{\max}} (t - t_0) + \tanh^{-1} \frac{v_0}{v_{\max}} \right] dt \quad (1.15)$$

Integrating from x_0 to x and from t_0 to t yields:

$$x - x_0 = \frac{v_{\max}^2}{b} \left\{ \ln \left[\cosh \left(\frac{b}{v_{\max}} (t - t_0) + \tanh^{-1} \frac{v_0}{v_{\max}} \right) \right] - \ln \left[\cosh \left(\tanh^{-1} \frac{v_0}{v_{\max}} \right) \right] \right\} \quad (1.16)$$

The equivalent process for $v_0 > v_{\max}$ is

$$\frac{dx}{dt} = v_{\max} \coth \left[\frac{b}{v_{\max}} (t_f - t_0) + \coth^{-1} \frac{v_0}{v_{\max}} \right] \quad (1.17)$$

Which is again separable into

$$dx = v_{\max} \coth \left[\frac{b}{v_{\max}} (t_f - t_0) + \coth^{-1} \frac{v_0}{v_{\max}} \right] dt \quad (1.18)$$

Integrating from x_0 to x and from t_0 to t yields:

$$x - x_0 = \frac{v_{\max}^2}{b} \left\{ \ln \left[\sinh \left(\frac{b}{v_{\max}} (t - t_0) + \coth^{-1} \frac{v_0}{v_{\max}} \right) \right] - \ln \left[\sinh \left(\coth^{-1} \frac{v_0}{v_{\max}} \right) \right] \right\} \quad (1.19)$$

During the coasting decent from apogee, Equations (1.11) and (1.16) apply with v_{\max} being replaced with v_t and b being replaced by $-g$.

The time from apogee to impact/landing is given by solving equation 1.16 from apogee to the ground for the time, and then using the time in Equation 1.11 to solve for the impact/landing velocity. For very long landing times, you may need to look up the inverse hyperbolic cosine in terms of natural log and use an approximate expression.

However, during the coasting ascent to apogee, Equation (1.6) becomes

$$a = -g \left(1 + \frac{v^2}{v_t^2} \right) \quad (1.20)$$

Which separates and integrates to

$$\tan^{-1} \frac{v}{v_t} - \tan^{-1} \frac{v_0}{v_t} = -\frac{g}{v_t} (t - t_0) \quad (1.21)$$

or

$$v = v_t \tan \left[\frac{-g}{v_t} (t - t_0) + \tan^{-1} \frac{v_0}{v_t} \right]. \quad (1.22)$$

To get the position, separate and integrate Equation (1.22).

$$x - x_0 = \frac{v_t^2}{g} \left(\ln \left\{ \cos \left[\frac{g}{v_t} (t - t_0) - \tan^{-1} \frac{v_0}{v_t} \right] \right\} + \ln \sqrt{1 + \frac{v_0^2}{v_t^2}} \right) \quad (1.23)$$

Apogee, and the time to apogee is found by setting the velocity to 0 in Equation (1.22), solving for the time to apogee and substituting into Equation (1.23).

$$0 = v_t \tan \left[\frac{-g}{v_t} (t_{\text{apogee}} - t_0) + \tan^{-1} \frac{v_0}{v_t} \right], \quad (1.24)$$

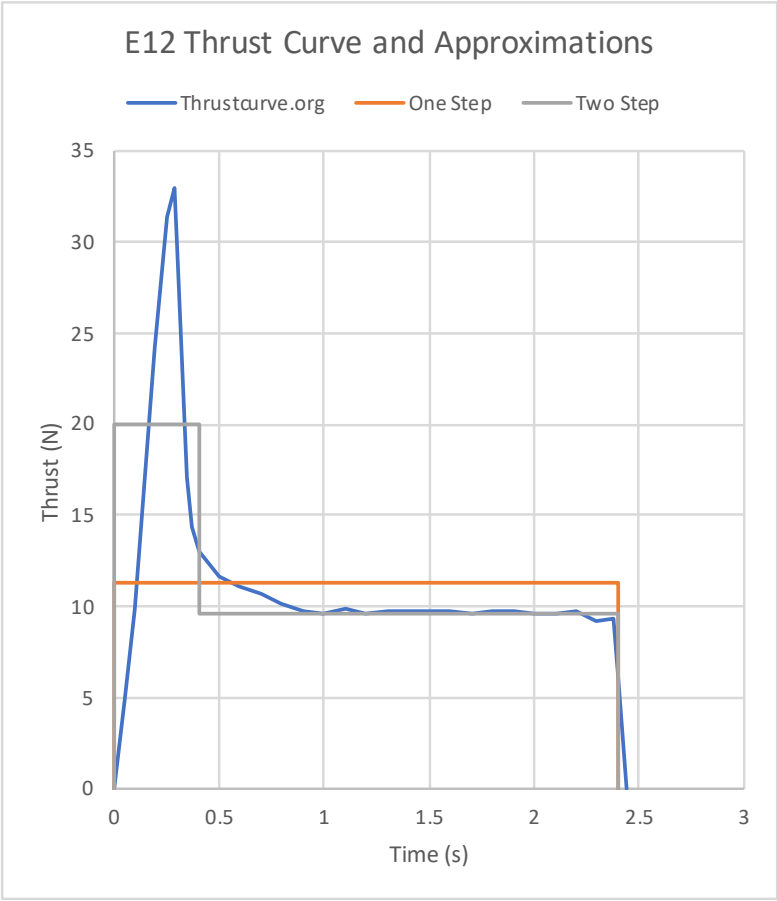
$$\frac{g}{v_t} (t_{\text{apogee}} - t_0) = \tan^{-1} \frac{v_0}{v_t}, \quad (1.25)$$

$$t_{\text{apogee}} - t_0 = \frac{v_t}{g} \tan^{-1} \frac{v_0}{v_t}, \quad (1.26)$$

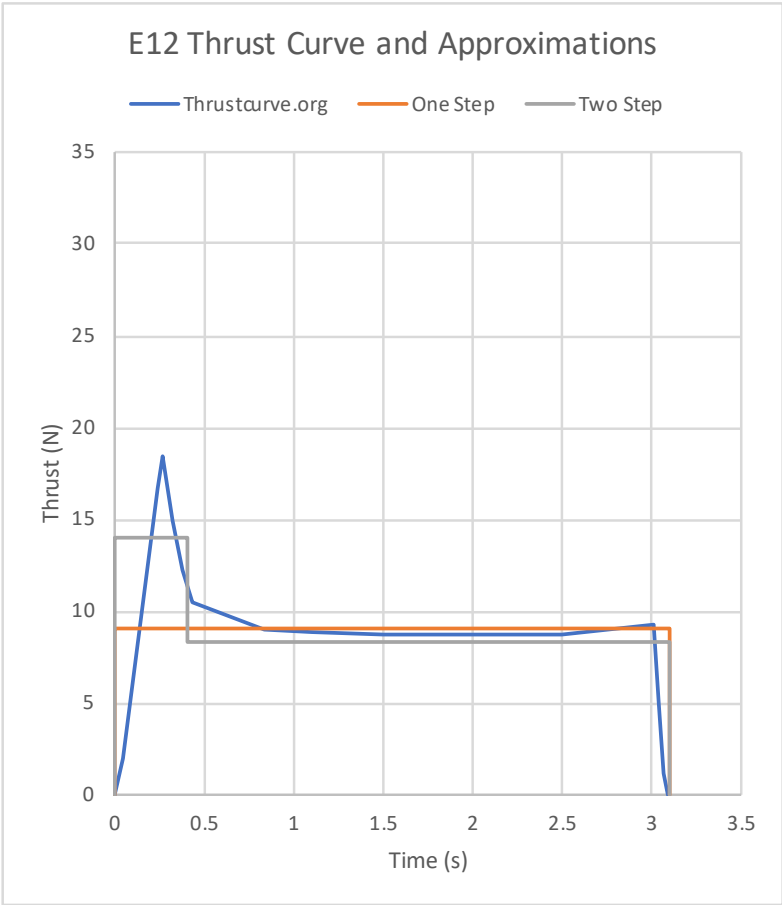
$$\begin{aligned} x_{\text{apogee}} - x_0 &= \frac{v_t^2}{g} \left(\ln \left\{ \cos \left[\frac{g}{v_t} \frac{v_t}{g} \tan^{-1} \frac{v_0}{v_t} - \tan^{-1} \frac{v_0}{v_t} \right] \right\} + \ln \sqrt{1 + \frac{v_0^2}{v_t^2}} \right) \\ &= \frac{v_t^2}{g} \left\{ \ln [\cos(0)] + \ln \sqrt{1 + \frac{v_0^2}{v_t^2}} \right\} = \frac{v_t^2}{g} \ln \sqrt{1 + \frac{v_0^2}{v_t^2}}. \end{aligned} \quad (1.27)$$













When implementing these equations in code, or when solving by hand, remember that they are piecewise function and that the final conditions for one segment, t_f , v_f , and x_f , are the initial conditions for the next segment, t_0 , v_0 , and x_0

Time (s)	Thrust (N)	Integral	Time (s)	Thrust (N)	Time (s)	Thrust (N)
0	0		0	0	0	0
0.052	5.045	0.13	1E-09	11.31	1E-09	20
0.096	9.91	0.46	2.4	11.31	0.4	20
0.196	24.144	2.16	2.4	0	0.4	9.57
0.251	31.351	3.69			2.4	9.57
0.287	32.973	4.85			2.4	0
0.3	29.91	5.26				
0.344	17.117	6.29				
0.37	14.414	6.70				
0.4	12.973	7.11				
0.5	11.712	8.35				
0.6	11.171	9.49				
0.7	10.631	10.58				
0.8	10.09	11.62				
0.9	9.73	12.61				
1	9.55	13.57				
1.101	9.91	14.55				
1.2	9.55	15.52				
1.3	9.73	16.48				
1.4	9.73	17.45				
1.5	9.73	18.43				
1.6	9.73	19.40				
1.7	9.55	20.36				
1.8	9.73	21.33				
1.9	9.73	22.30				
2	9.55	23.26				
2.1	9.55	24.22				
2.2	9.73	25.18				
2.3	9.19	26.13				
2.375	9.37	26.83				
2.4	5.95	27.02				
2.44	0	27.14				
		11.31				



Time (s)	Thrust (N)	Integral	Time (s)	Thrust (N)	Time (s)	Thrust (N)
0	0		0	0	0	0
0.046	1.913	0.04	1E-09	9.05	1E-09	14
0.235	16.696	1.80	3.1	9.05	0.4	14
0.273	18.435	2.47	3.1	0	0.4	8.32
0.326	14.957	3.35			3.1	8.32
0.38	12.174	4.09			3.1	0
0.44	10.435	4.77				
0.835	9.043	8.61				
1.093	8.87	10.92				
1.496	8.696	14.46				
1.997	8.696	18.82				
2.498	8.696	23.18				
3.014	9.217	27.80				
3.037	5.043	27.96				
3.067	1.217	28.06				
3.09	0	28.07				
		9.05				



Components	Status
<div data-bbox="495 724 711 766">  Sustainer </div> <div data-bbox="568 777 820 819">  Nose cone </div> <div data-bbox="544 829 812 871">  Body tube </div> <div data-bbox="625 871 909 913">  Tube coupler </div> <div data-bbox="625 924 876 966">  Launch lug </div> <div data-bbox="625 966 787 1008">  Mass </div> <div data-bbox="641 1018 868 1060">  Parachute </div> <div data-bbox="544 1071 812 1113">  Body tube </div> <div data-bbox="625 1113 868 1155">  Body tube </div> <div data-bbox="625 1155 925 1197">  Centering ring </div> <div data-bbox="625 1207 925 1249">  Centering ring </div> <div data-bbox="625 1260 820 1302">  Fin set </div>	

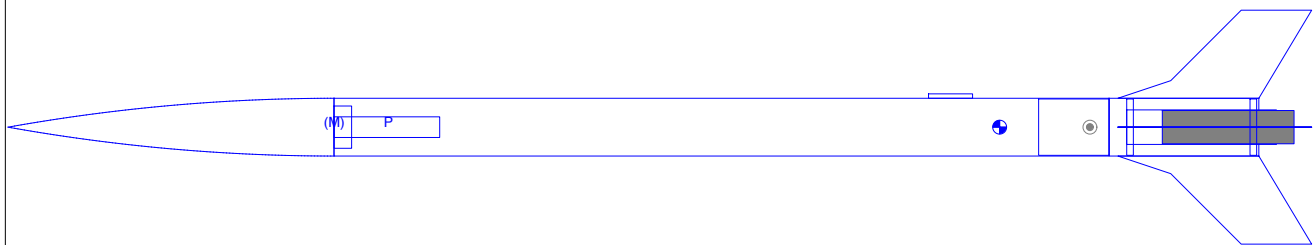
Albee Vector Vehicles Model 01D

Length: 37.0000 In. , Diameter: 1.6400 In. , Span diameter: 6.6400 In.

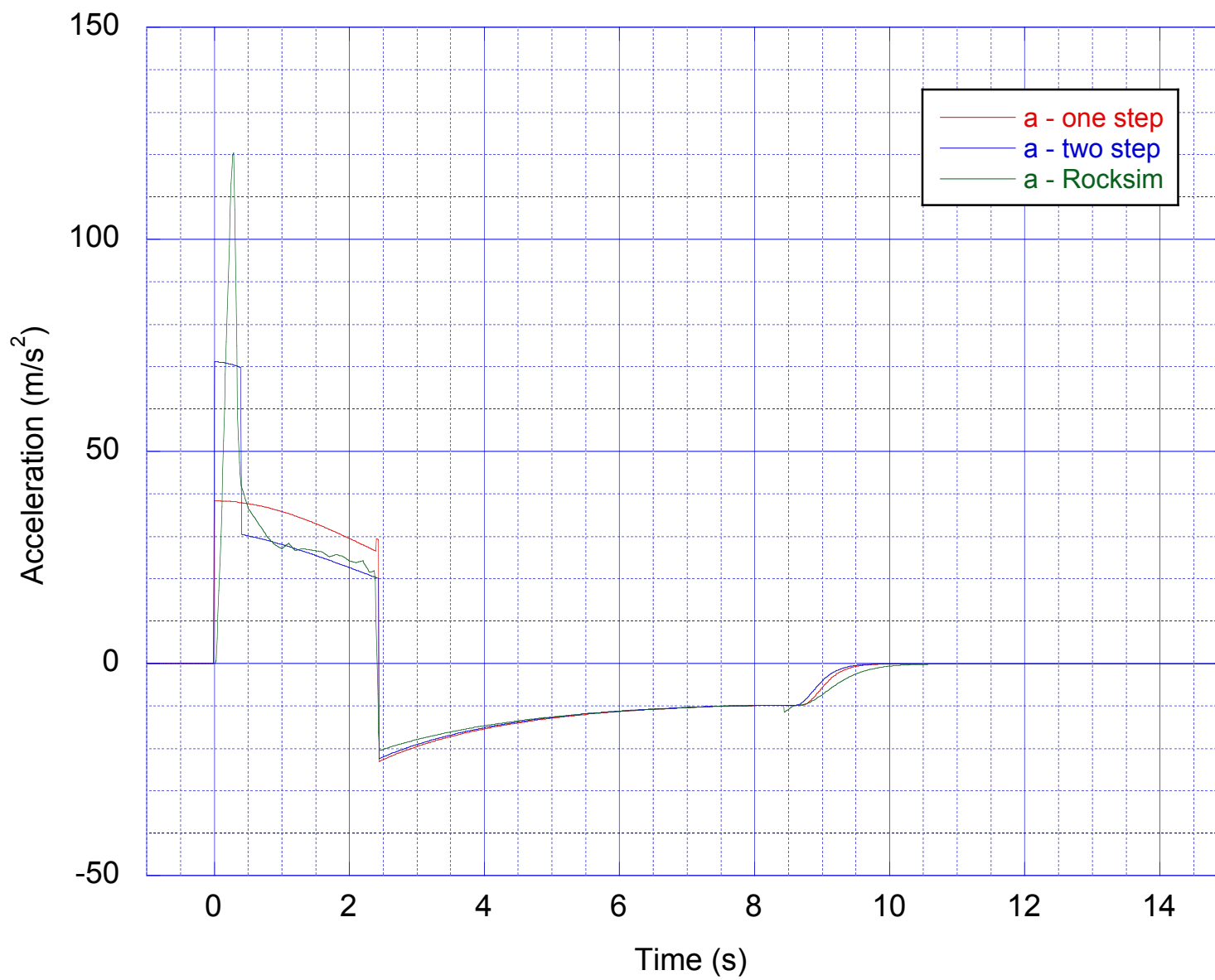
Mass 260.100 g , Selected stage mass 260.100 g (User specified)

CG: 28.1434 In., CP: 30.7061 In., Margin: 1.56

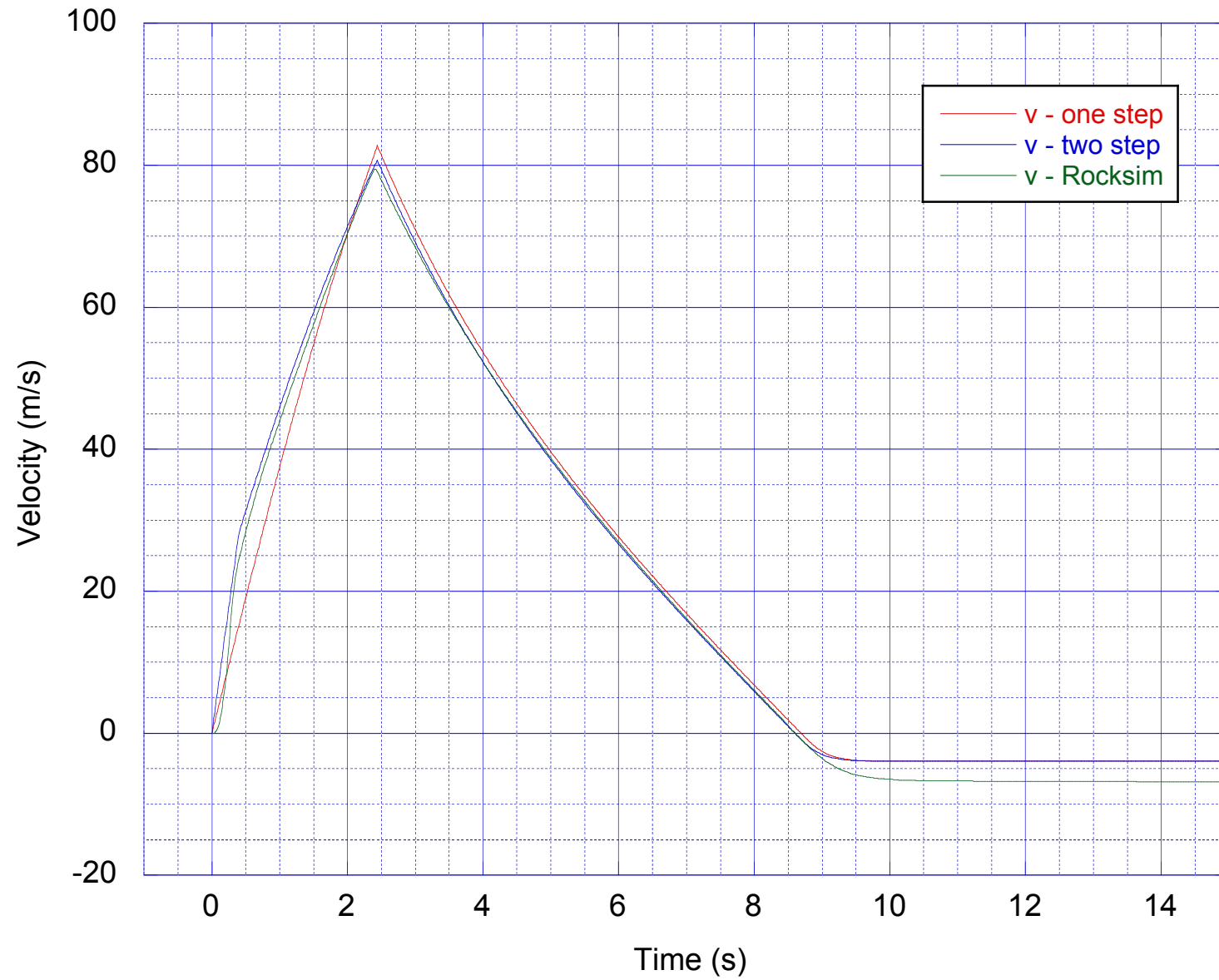
Engines: [E9-8,]



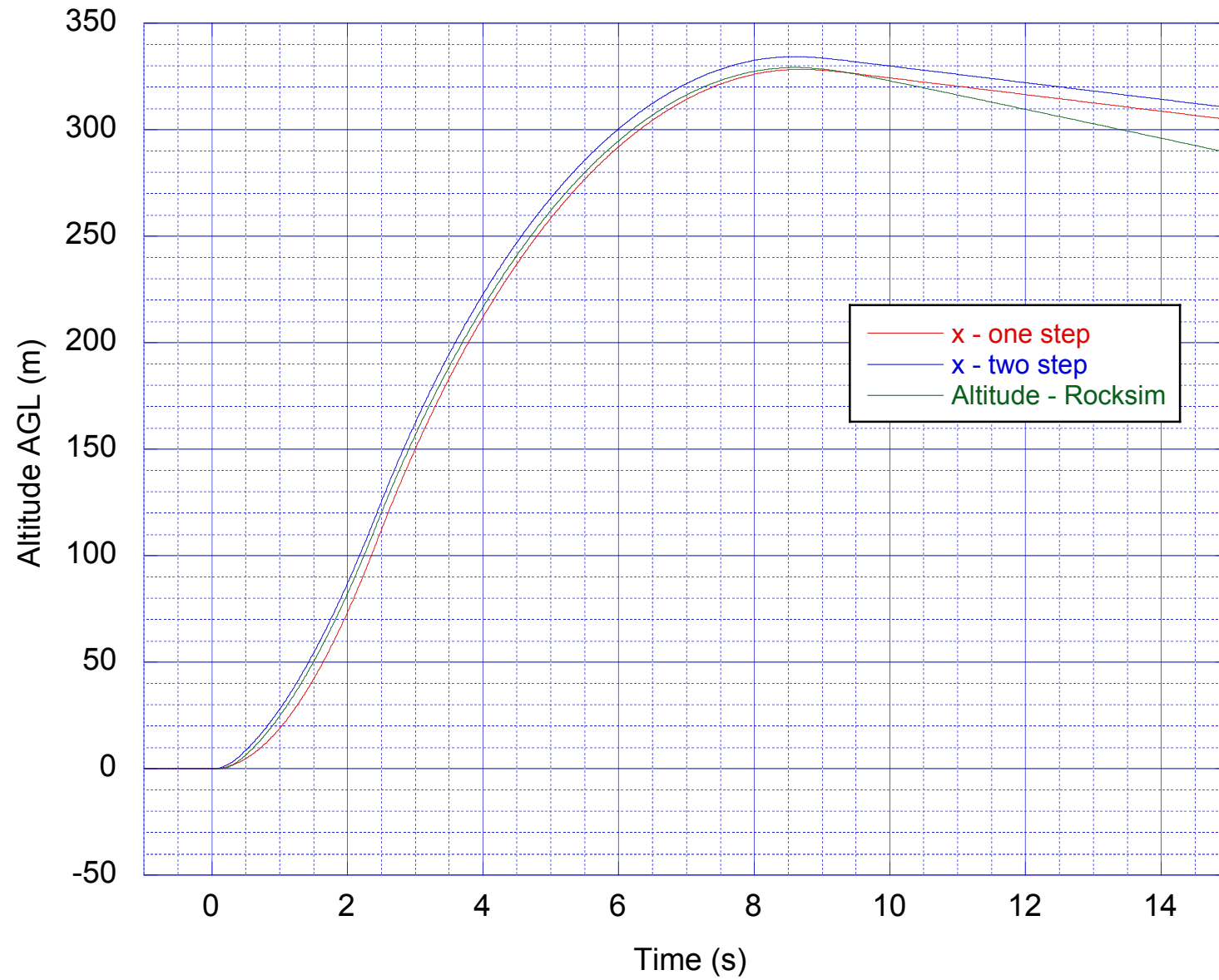
E12 Acceleration Data



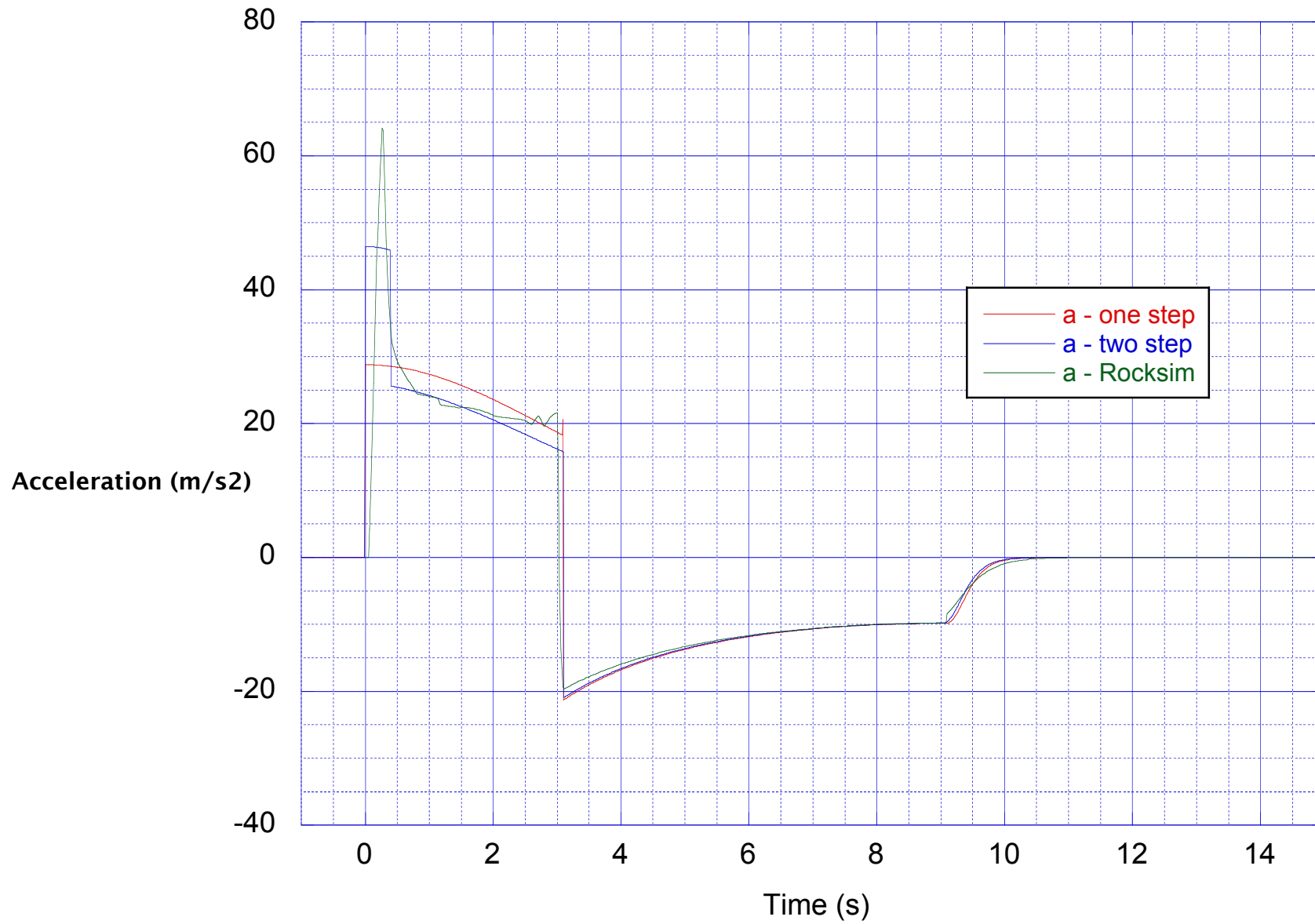
E12 Velocity Data



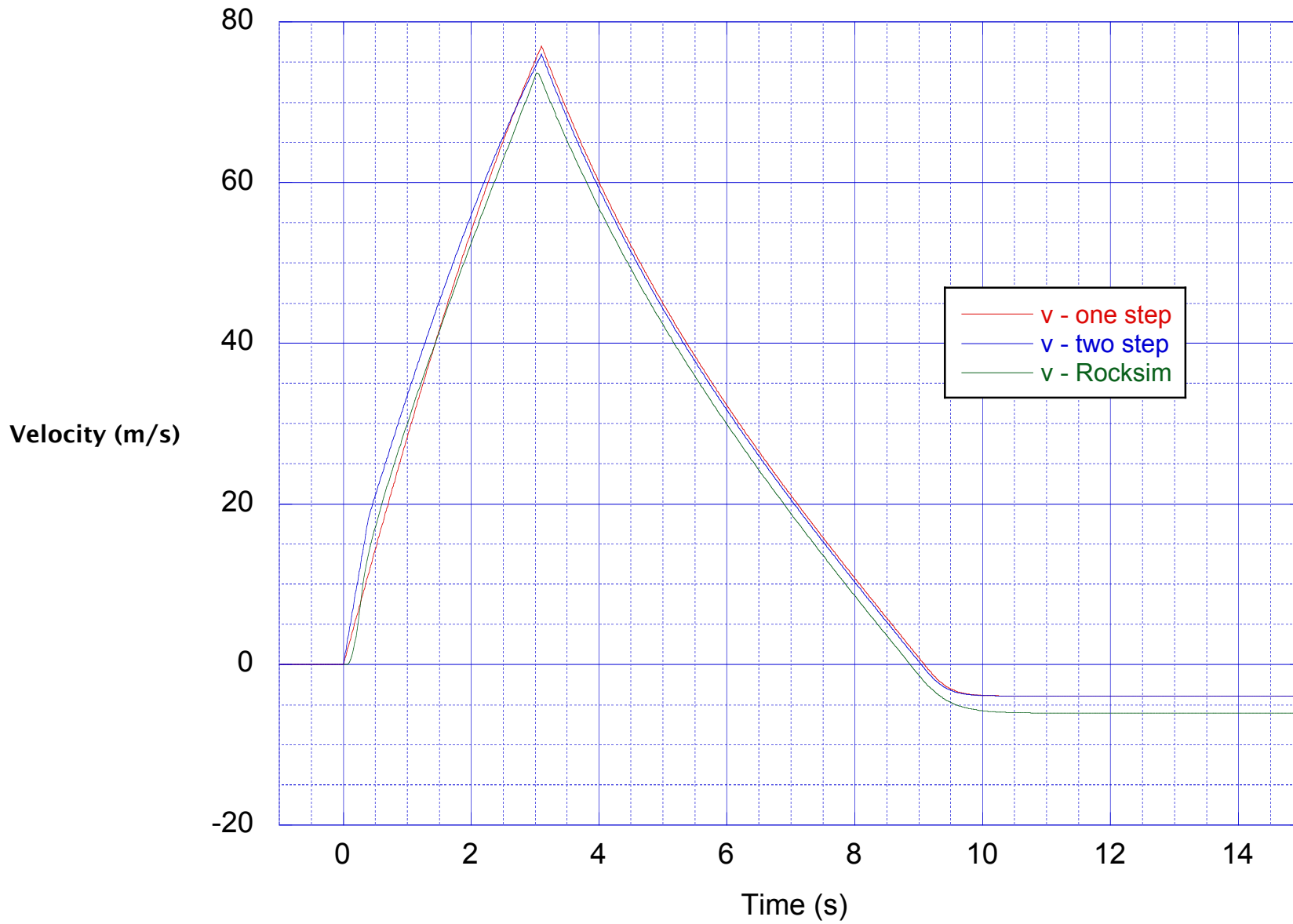
E12 Altitude Data



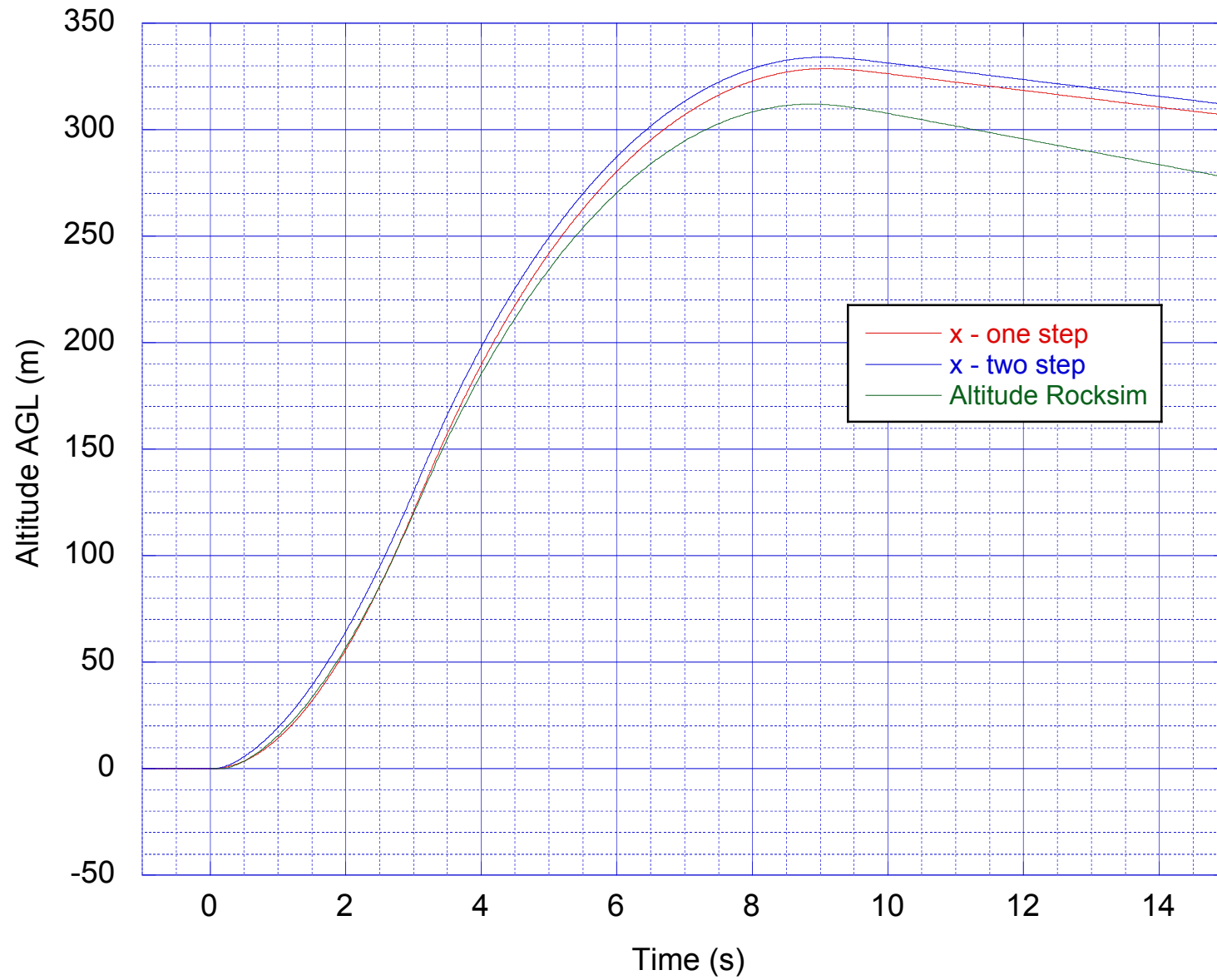
E9 Acceleration Data



E9 Velocity Data



E9 Altitude Data



E9

One Step Model		Two Step Model	
tdelay =	5.994	tdelay =	5.9401
tapogee =	9.094	tapogee =	9.0401
apogee =	327.8866	apogee =	334.1189
tim pact =	337.2571	tim pact =	343.4355
vim pact =	-3.911	vim pact =	-3.911

E12

One Step Model		Two Step Model	
tdelay =	6.2402	tdelay =	6.0885
tapogee =	8.6802	tapogee =	8.5285
apogee =	326.3895	apogee =	327.0155
tim pact =	335.3455	tim pact =	335.8198
vim pact =	-3.9019	vim pact =	-3.9019