

E151 Lecture 18 – Open and Short Circuit Time Constants

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Disclaimer

These are notes for Prof. Spencer to give the lecture, they were not intended as a reference for students. Students asked for them anyway, so I'm putting them up as a courtesy. Remember that they are not intended as a substitute for attending lecture.

Lab Debrief

- AC coupling
 - We're not modeling it in our TF right now, low f will be wrong
 - step responses: see dynamics right close to edge
- Extracting C_{mu} and C_{pi}
 - assume $C_{ce}=0$, $C_{ob0}=C_{mu}$, use fT to get C_{pi}
 - OR, use $C_{ib0} + \tau_F$ and g_m
- Some weirdness in this lab measuring r_{in} and r_{out} ... play around a bit
- Make sure to record phase for Bode plots
- MAKEUP LAB HOURS on Wednesday, 6-9PM

Full TF Hard (no good Z_{th}) & Miller has issues

- Miller issues: CE specific and non-conservative, but insightful
- We Want
 - a general approximation method that works for any circuit
 - approximation to be conservative & to lend design insight
 - a technique that can be used to calculate f_{low}
- Open circuit time constants & short circuit time constants (O/SCTC)
 - Invented at MIT in the 60s

What are OCTC?

- Assume our transfer function has a mid-band
- Focus on finding first pole accurately (assume widely separated)
- “zero-causing caps” are going to be shorted at this frequency



Real CE: $H(s) = A_v \frac{(1 - s/z_1)}{(1 - s/p_1)(1 - s/p_2)}$ Moller: $H(s) = A_v \frac{1}{1 - s/p_n}$ ← lose info, use ZTH of C_n to get p_n

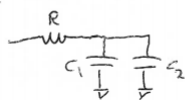
$$OCTC: H(s) = A_v \frac{1}{(1 - s/p_1)(1 - s/p_2) \dots (1 - s/p_n)} = A_v \frac{1}{1 + \underbrace{\left(\frac{1}{p_1} + \frac{1}{p_2} + \dots + \frac{1}{p_n}\right)}_{\text{same as } \tau_1 + \tau_2 + \dots} s + \dots + \underbrace{\left(\frac{1}{p_1 p_2 \dots p_n}\right)}_{\text{same as } \tau_1 \tau_2 \dots \tau_n} s^n}$$

$$H(s) \approx A_v \frac{1}{1 + (\tau_1 + \tau_2 + \dots + \tau_n)s} \quad \text{Because } \tau_n \text{'s small @ corner for } n > 2$$

Fine, but I don't know τ_i

- Can't Thevenize @ caps b/c the caps communicate in general
- **Big result:** $\sum_{i=0}^n \tau_i = \sum_{i=0}^n OCTC_i$ where $OCTC_i = C_i R_{th,i} | C_{k \neq i} \text{ open}$
- Exactly predicts first pole in OCTC TF
- Only include “pole-causing” caps in analysis b/c “zero causing” short

Example (trivial)



Exact

$$\tau = R(C_1 + C_2)$$

OCTC

$$OCTC_1 = C_1 R$$

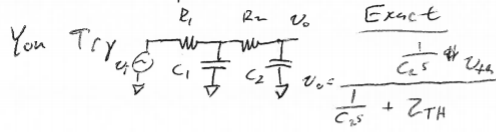
$$OCTC_2 = C_2 R$$

$$\sum OCTC = R(C_1 + C_2)$$

- Expect 1st order to work perfectly based on TF

Less Trivial Example

Less trivial example



$$Z_{TH} = R_2 + R_1 \parallel \frac{1}{C_1 s}$$

$$= R_2 + \frac{R_1}{1 + R_1 C_1 s}$$

vs. OCTC

$$OCTC_1 = C_1 R_1$$

$$OCTC_2 = C_2 (R_1 + R_2)$$

$$3_{dB} @ (R_1 C_1 + (R_1 + R_2) C_2)^{-1}$$

$$\frac{v_0}{v_1} = \frac{\frac{1}{C_2 s} - \frac{1}{1 + R_1 C_1 s}}{\frac{1}{C_2 s} + R_2 + \frac{R_1}{1 + R_1 C_1 s}}$$

$$v_{TH} = \frac{1/C_1 s}{R_1 + 1/C_1 s} v_1 = \frac{v_1}{1 + R_1 C_1 s}$$

$$= \frac{1}{(1 + R_1 C_1 s) + R_2 C_2 s (1 + R_1 C_1 s) + R_1 C_2 s^2 + R_1 C_1 s}$$

$$\dots + R_1 C_1 s \rightarrow (1 + \frac{1}{p_1}) (1 + \frac{1}{p_2})$$

- Works for p1! Esp. good if $\tau_1 > \tau_2 \rightarrow$ Miller helps

Failure Mode if Poles are Closely Spaced

— what happens if poles are close?

$$\frac{1}{1 + (\tau_1 + \tau_2)s + \tau_1 \tau_2 s^2} \xrightarrow{FRF} \frac{1}{1 + (\tau_1 + \tau_2)\omega_{-3dB, est} + \tau_1 \tau_2 \omega_{-3dB, est}^2}$$

= 1 by def of OCTC

each of $\tau_1 + \tau_2$ must be < 1 , so product much smaller
 Worst case, $\tau_1 = \tau_2 \rightarrow$ this is $\frac{1}{4(\tau_1 + \tau_2)\omega_{est}^2}$

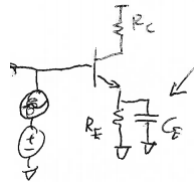
— Also, even if this doesn't give us the exact

ω_{-3dB} , it does give us \rightarrow ① a good guess

\rightarrow ② design insight about which caps cause trouble

Try a CE + a pattern for Cmu

- Ignore Ce and coupling caps b/c zero-causing, not pole-causing



You guys find OCTC_π
 $= (R_{\pi} || R_{TH}) C_{\pi}$

- Cmu is more complicated:

Compare

Exact
 $Z_1 = C_{\mu} R + C_{\pi} (R + R_{\pi} + R_{TH})$

Miller
 $Z_1 = C_{\mu} R + C_{\pi} (R + \beta R_{TH})$

We went Miller!

SCTC

- Not associated w/ particular zero
- Pole-causing caps open
- Find f_{low}
- Find 2nd order pole w/ OCTC

OCTC reminder

$$\text{Let } H(s) = \frac{A_V}{(1 + z_1 s)(1 + z_2 s) \dots (1 + z_n s)} = \frac{1}{(1 + z_1 s) \dots (1 + z_n s)}$$

$$= \frac{A_V}{1 + s \sum z_i + \dots + \prod z_i \cdot s^n}$$

Asses low order terms matter b/c @ high f close to z_i

SCTC

$$\text{Let } H(s) = \frac{A_V k s^k}{(s + p_1)(s + p_2) \dots (s + p_n)} = \frac{A_V k s^k}{s^n + s^{n-1} \sum p_i + \dots + \prod p_i}$$

Alternate form of poles, need k + $\prod p_i$
 High pass - like behavior

Asses high order terms matter b/c @ $\frac{\prod p_i}{s^{n-1}}$ small at low f near corner

$$\text{so } H(s) = \frac{A_V k s}{s + \sum p_i}$$

pole located @ sum of pole frequencies, still tend to find

$$\sum z_i = \sum \text{OCTC}_i$$

where $\text{OCTC}_i = C_i \cdot R_{TH}$ | caps open

$$\sum p_i = \sum \text{SCTC}_i^{-1}$$

where $\text{SCTC}_i = C_i \cdot R_{TH}$ | All other caps short