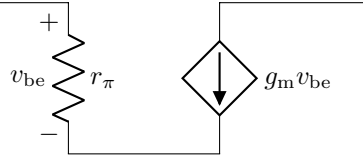


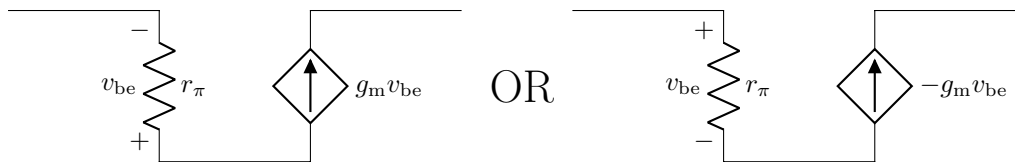
# Small-Signal Tricks

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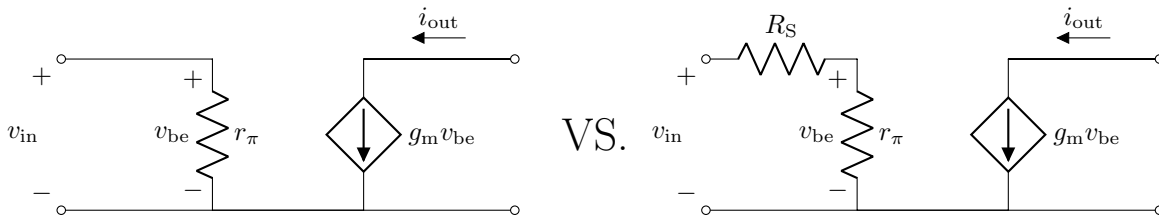
**Flipping Direction** Consider the following simple small-signal model:



Sometimes, it's convenient to flip the direction of the voltage-controlled current source (for instance, to match one of the other tricks in this handout). In this case,  $v_{be}$  must be flipped too, either on  $r_\pi$  or in the voltage-controlled current source's equation:



**Effective  $g_m$**  Compare the simple small-signal model of the previous trick with one with a source resistance:



In the left circuit,  $v_{be} = v_{in}$ , and so the output current is simply

$$i_{out} = g_m v_{be} = g_m v_{in}.$$

However, in the right circuit,  $v_{be}$  is divided such that  $v_{be} = \frac{r_\pi}{R_S + r_\pi} v_{in}$ . The output current will be similarly divided:

$$i_{out} = g_m v_{be} = \frac{r_\pi}{R_S + r_\pi} g_m v_{in}.$$

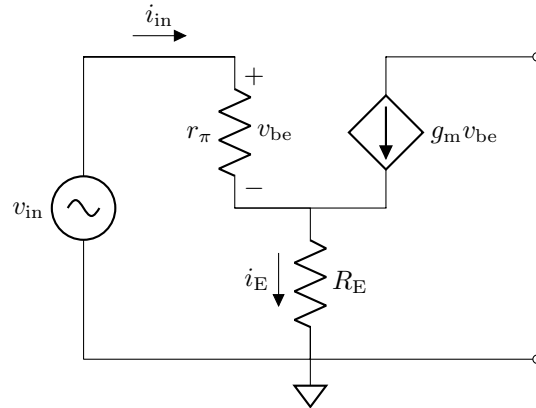
Evidently, adding the source resistance decreased the amplification power of the transistor. To quantify this effect, we lump the division factor into  $g_m$  to make an effective  $g_m$ :

$$g_{m,\text{eff}} = \frac{r_\pi}{R_S + r_\pi} g_m.$$

Now, just as before, the amplification of the transistor is written as  $i_{out} = g_{m,\text{eff}} v_{in}$ . Thinking about effective  $g_m$  can give quick intuition about the effect that dividing  $r_\pi$  has on an amplifier's gain.

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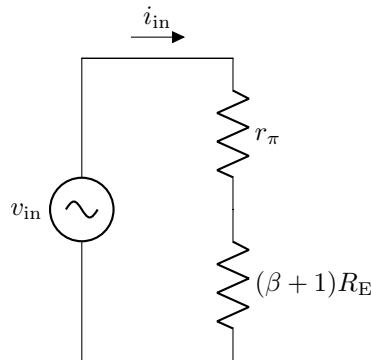
**Boosting  $R_E$**  Consider the following circuit:



Let's say we're trying to find  $r_{in}$ , meaning we only care about the ratio between  $v_{in}$  and  $i_{in}$ . To calculate  $v_{in}$ , we really only need to find  $i_E$  since  $v_{in} = i_{in}r_{\pi} + i_E r_E$ . We find  $i_E$ :

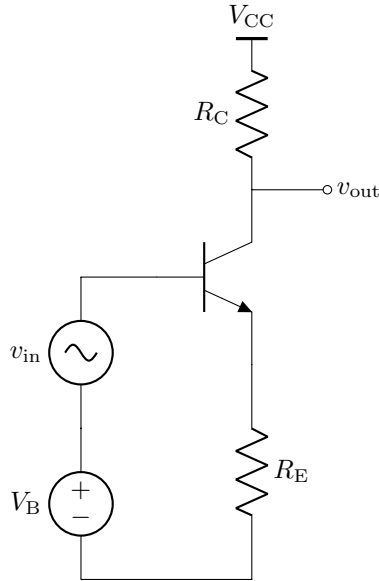
$$i_E = i_{in} + g_m v_{be} = i_{in} + g_m i_{in} r_{\pi} = (\beta + 1)i_{in}.$$

Interestingly, this is the same current that would flow through a resistor of size  $(\beta + 1)R_E$  without the voltage-controlled current source. This allows us to transform the circuit as follows:

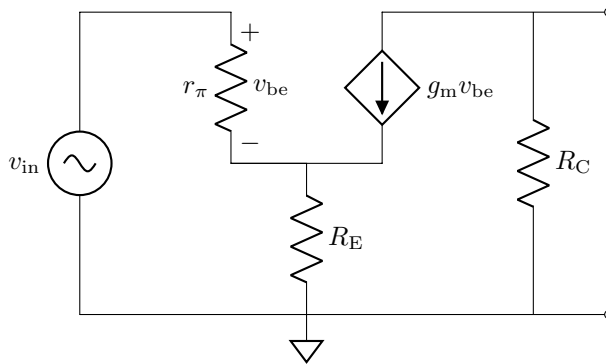


Here,  $r_{in}$  is trivial to solve for. So, we see that a  $g_m$  generator driving into  $R_E$  effectively increases its resistance by a factor of *beta*. Making this substitution can greatly simplify complicated small-signal models.

As an example of this trick, consider a common emitter amplifier with emitter degeneration:



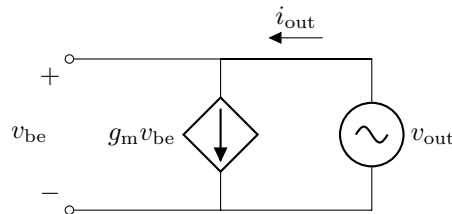
The small-signal model becomes



$R_C$  doesn't affect  $r_{in}$ , so this circuit is the same as that at the beginning of this trick for finding  $r_{in}$ . Making the  $(\beta + 1)R_E$  substitution, we find

$$r_{in} = (\beta + 1)R_E + r_{\pi}.$$

**Directly Wiggling  $g_m$**  Consider the following circuit:

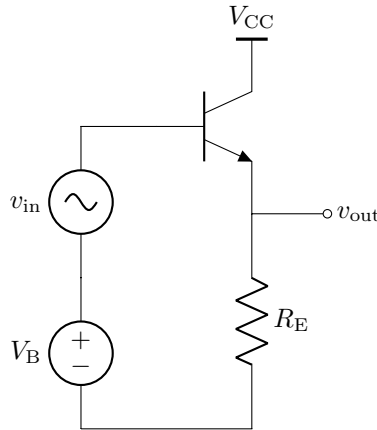


Let's say we're trying to find  $r_{out}$ . Because we're driving  $v_{be}$ , the voltage-controlled current source will output a current directly proportional to  $v_{out}$ . And, since our output ports are directly across this current source, its current equals  $i_{out}$ . Then, we simply have

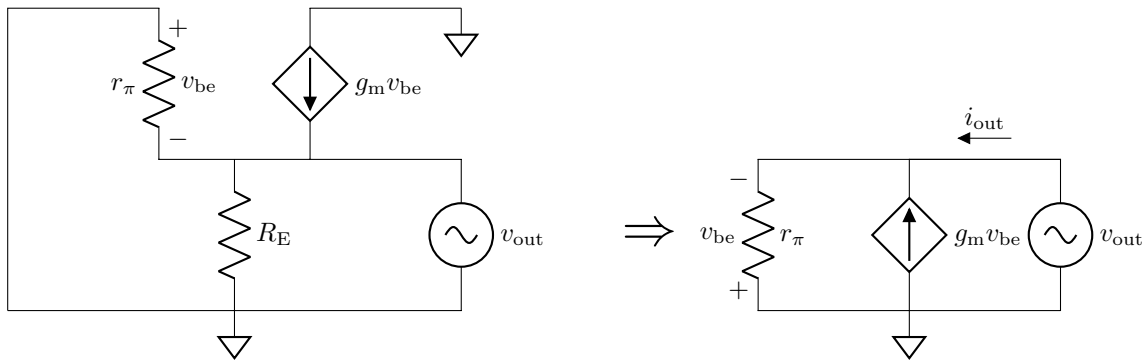
$$r_{out} = \frac{v_{out}}{i_{out}} = \frac{v_{out}}{g_m v_{out}} \Rightarrow \boxed{r_{out} = \frac{1}{g_m}}.$$

The intuition behind this is that we directly control the wiggle on  $v_{be}$ , which  $g_m$  is related to. So,  $r_{out}$  depends directly on  $g_m$ .

As an example, consider finding  $r_{out}$  of an emitter follower:



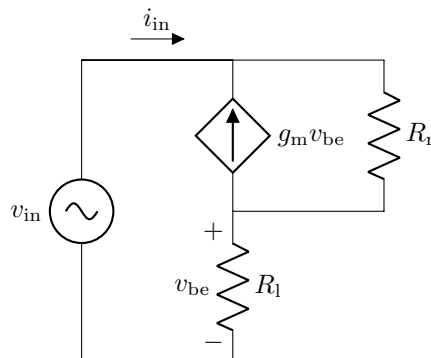
The small-signal model for finding  $r_{out}$  (ignoring  $r_o$ ) is



We can assume that very little current flows through  $r_\pi$  as compared with the voltage-controlled current source. We can also use the "flipping direction" trick so that the voltage-controlled current source points down and  $v_{be}$  is flipped. Then, this circuit perfectly matches the circuit for wiggling  $g_m$ , and we find

$$r_{out} \approx \frac{1}{g_m}.$$

**Left-Right Pattern for  $r_{in}$**  Consider the following circuit:



In this topology, we call  $R_l$  the left resistor and  $R_r$  the right resistor. We solve for  $r_{in}$  for this circuit:

$$v_{be} = i_{in} R_l \tag{1}$$

KCL @ top node:

$$i_{in} = -g_m v_{be} + \frac{v_{in} - v_{be}}{R_r}$$

Substituting in (1):

$$i_{in} = -g_m i_{in} R_l + \frac{v_{in} - i_{in} R_l}{R_r}$$

Multiply through by  $R_r$  :

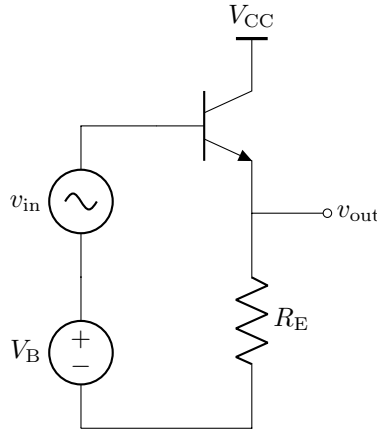
$$R_r i_{in} = -g_m i_{in} R_l R_r + v_{in} - i_{in} R_l \tag{2}$$

$$\Rightarrow v_{in} = i_{in} (R_l + R_r + g_m R_l R_r)$$

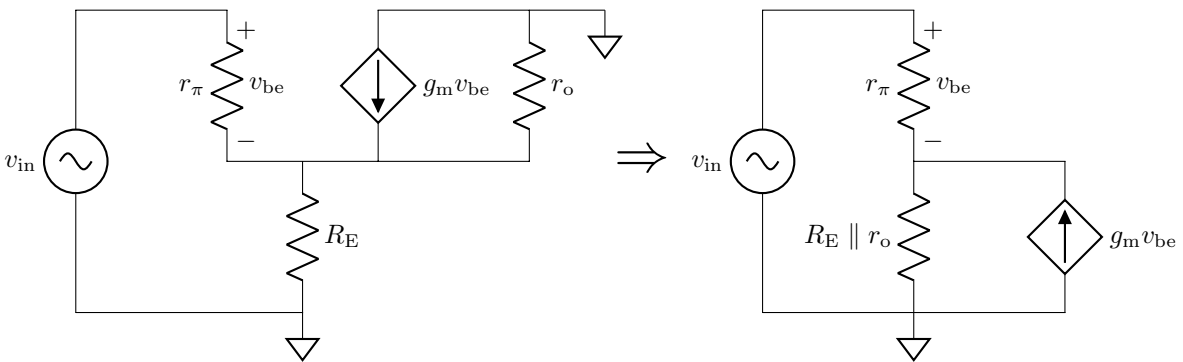
Substituting in (2):

$$r_{in} = \frac{v_{in}}{i_{in}} \Rightarrow \boxed{r_{in} = R_l + R_r + g_m R_l R_r}$$

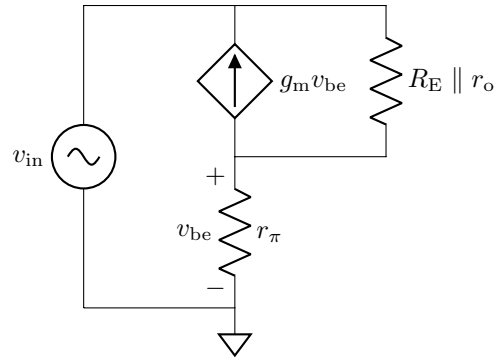
This pattern shows up surprisingly often, allowing the input resistance to be read off instead of derived. For example, consider a simple emitter follower. If we ignore any source and load resistance, we have:



The small signal model becomes



$r_{\pi}$  is in series with the bottom half of the circuit, so we can simply switch these two halves:



Using the left-right trick for  $r_{\text{in}}$ , we find by inspection that

$$r_{\text{in}} = r_{\pi} + R_{\text{E}} \parallel r_{\text{o}} + g_{\text{m}} r_{\pi} R_{\text{E}} \parallel r_{\text{o}} = (\beta + 1)(R_{\text{E}} \parallel r_{\text{o}}) + r_{\pi}.$$