

Output Stage & Incidence & Review

- Clarity emails
- Why does A loaded EF clip?
- Lab test setup & a fair comparison
- backstab... etc.

Op-amp summary

- Have diff input & low Z_o
- Need to gain \rightarrow Gain stage
- Tend to put in feedback, use cure

What is stability?

- No oscillations definition \rightarrow vs. non-linearity
- Passive systems don't oscillate
- Accidental vs. purposeful EB & spotting stability

Root Locus Intro

- L(s) setup
- True gain & steady-state error
- Open-loop vs closed loop gain & poles
- Want to work w/ L(s) 6.101-4

Gain & Phase Margin

- Link between Bode & crossing to RHD
- Define ϕ margin (covers) (covers)
- Compensation
- Max cap load

9.2-3

- Before we start I want to take any Qs you have about output stages and emails

\rightarrow where does power come from if not V_{dd} \rightarrow MPTT clear up control L: make S control S : make $Z=0$

- We also need to visit impedances in output stages in more detail
- only one device or in push-pull or class AB
- looks like weird EF w/ according R_{in} & R_{out} , pick V_{B1n} as avg?

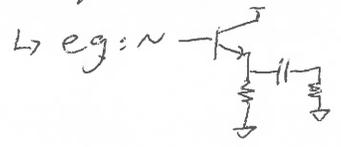


\rightarrow need to compare linear spots where amp is on \rightarrow eg: $V_2 = (V_1 - 0.7) \cdot \frac{R_L}{R_{out} + R_L}$ & need to correct -0.7 shift

- Class AB like +ve or -ve EF, comes w/ I_B so can get eg: $g_m |_{I_B}$

- Fair comparisons

- \rightarrow compare linearity under same power delivery \leftarrow critical plan
- \rightarrow compare under constant input \leftarrow easier
- \rightarrow you don't need to fix non-linearity, just explain it

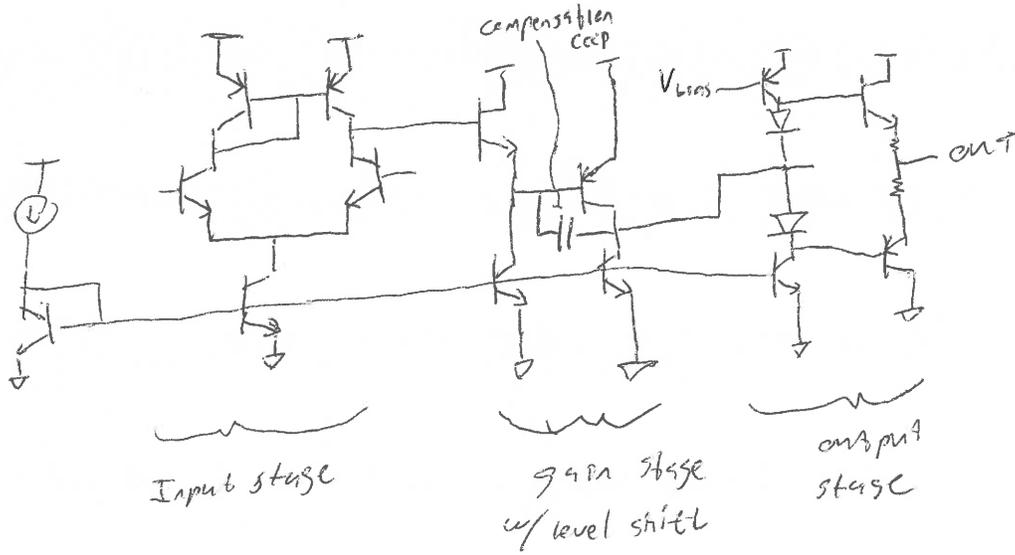


$$i_L = i_E + i_L$$

$$I_S e^{(V_{be} - V_c)/kT} = \frac{v_E(t)}{R_E} + \frac{v_c(t) - v_E(t)}{R_E}$$

- numerical solve $\rightarrow v_E(v_b)$
- competing effects @ v_E

- Op-amps have 3 things:
 - diff input w/ high Z_{in} ✓
 - infinite gain ✓
 - zero Z_{out} ✓



- DC coupled & uses a level shift
- slow rate
- Compensation cap
 - Big millifarad cap \rightarrow small BW
 - why there?

- Almost always use op-amps in feedback which has big implications for gain stage

- That's b/c any time you hear "feedback" \rightarrow think "risk of instability"

What is stability

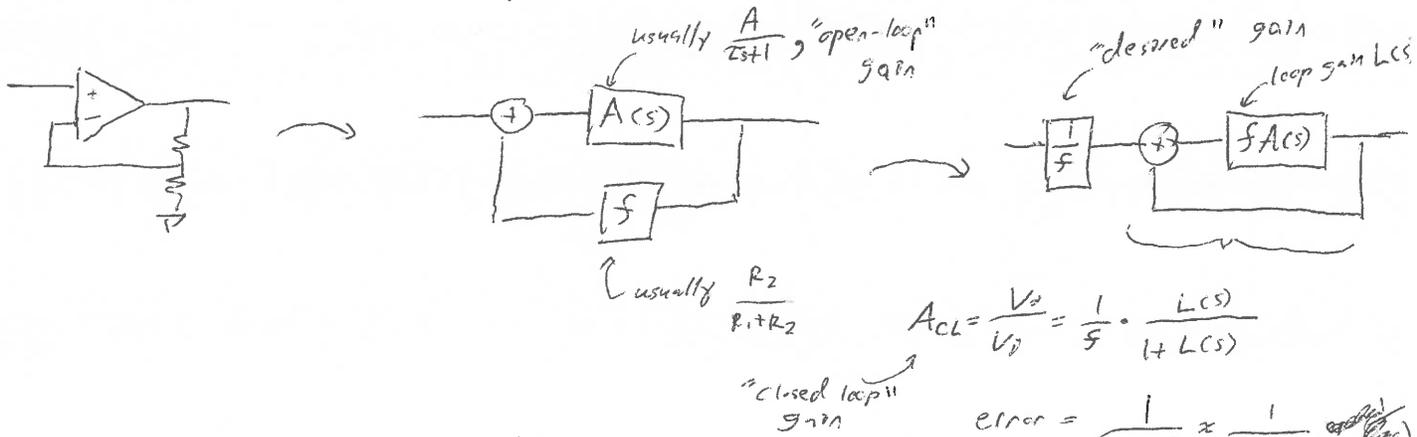
- \hookrightarrow lots of formal definitions: Lyapunov, Nyquist, BIBO
- \hookrightarrow for us, means: does not latch up & does not oscillate (ok for engineers)
- \hookrightarrow can see in f domain: only see energy @ f we put in (+ harmonics if non-linear)

Oscillations come from poles on imaginary axis

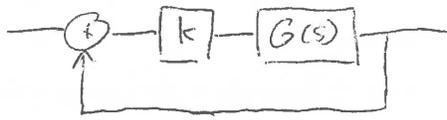
- \hookrightarrow poles might swing to RHP & back to LHP ~ describing functions
- \hookrightarrow but our amps have LHP poles (exact analysis)
- \hookrightarrow feedback moves poles (example in a second)
- \hookrightarrow we have parasitic feedback ~ load rags & make v_{in} big ~ supply moves

tiny
 \checkmark have high f excitation @ all times

Tiny intro to root locus techniques



• root-locus techniques designed for P control system



Let $G(s) = \frac{G}{s+1}$, note $L(s) = kG(s)$

$$\frac{N_o}{V_i} = \frac{\frac{kG}{s+1}}{1 + \frac{kG}{s+1}} = \frac{kG}{s+1+kG} = \frac{k}{1+k} \cdot \frac{1}{\frac{s}{k+1} + 1}$$

error from here

pole has moved!

- can draw pictures showing how pole moves called root-locus diagrams

- Good @ drawing diagrams lets us reason about $L(s)$ (usually well known) w/o thinking about $A_{CL}(s)$ (usually pain in butt)

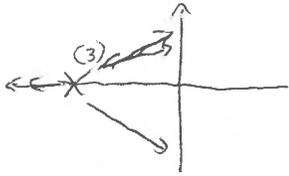
- Aside: in op-amp example $A_{CL} \approx \frac{1}{F}$ & pole location $\approx \frac{\tau}{A\tau}$ ($k=A\tau$)

↳ smaller F increases τ & increases gain

↳ leads to constant gain-bandwidth product ← result of 1st order roll-off in op-amps

↳ $\tau = \frac{1}{\omega_c}$ so $\omega_c = \frac{A\tau}{\tau}$. $\omega_c \cdot A_{CL} = \frac{A\tau}{\tau} \cdot \frac{1}{F} = \frac{A}{\tau}$ ← constant! pick BW if setting A_{CL} closed-loop

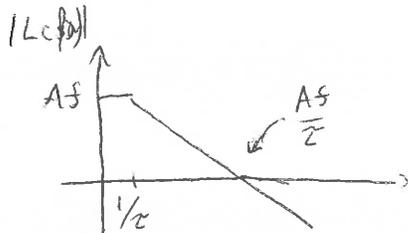
- we don't have full root-locus training, want fast way to get from L(s) to stability
- circuit design done w/ awesome hack called phase margin



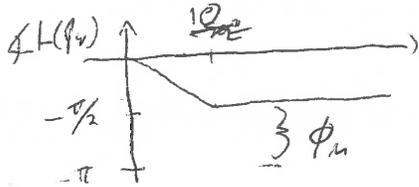
- case where closed loop poles are on $j\omega$ axis or RHP
- Definitely unstable if $L(s) = -1$ w/c $A_{CL} \rightarrow \infty$
- If becoming unstable, poles crossing imaginary axis
- can find $L(j\omega) = -1$ to get instability, comes from Bode.

Can easily find $L(j\omega) = -1 \rightarrow |L(j\omega)| = 1$ & $\angle L(j\omega) = -\pi$

- Look for $|L(j\omega)| = 1$ on Bode plot ... called crossover



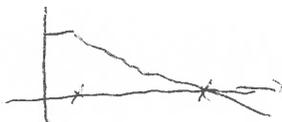
- (crossover corresponds to non-unity gain in feedback loop comprised of L(s) \rightarrow rolloff in A_{CL})



- Distance from 180° of phase @ crossover is your phase margin
- How far are you from crossing imaginary axis? \sim v. dicey in conditionally stable systems

\rightarrow positive ϕ_m usually means stable \leftarrow

You try ~ system w/ 2 widely spaced poles, 2nd pole @ crossover



- can relate ϕ_m to peak overshoot
- 45° very modest $\rightarrow Q = 3$ or $\zeta = 0.12$



$\phi_m = 45^\circ$ ~ classy point

Coming up

- feedback applications \rightarrow oscillators!
- why do -p-amps look like 1 pole? ie: what is the virtue of compensation cap?